



20<sup>TH</sup> INTERNATIONAL  
CONFERENCE ON  
CARBON DIOXIDE  
UTILIZATION 2023

ENHANCED CO<sub>2</sub>  
CAPTURE USING  
SODA SOLUTION

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# Background & Motivation

- CO<sub>2</sub> Capture by other methods are quite expensive and complex in treatment
- Na<sub>2</sub>CO<sub>3</sub> solution is less corrosive and environment friendly than amines
- Na<sub>2</sub>CO<sub>3</sub> solution can be regenerated using low temperature heat (< 70°C) in vacuum while amines need steam for regeneration
- 8 w-% Na<sub>2</sub>CO<sub>3</sub> solution is better than water for absorbing CO<sub>2</sub> since absorption capacity of water is low and need cooling to lower temperature but the limitation of Na<sub>2</sub>CO<sub>3</sub> solution is slow mass transfer than amines
- The knowledge of accurate absorption rate of CO<sub>2</sub> capture using soda solution employing a device to generate bubbles is not available in other research



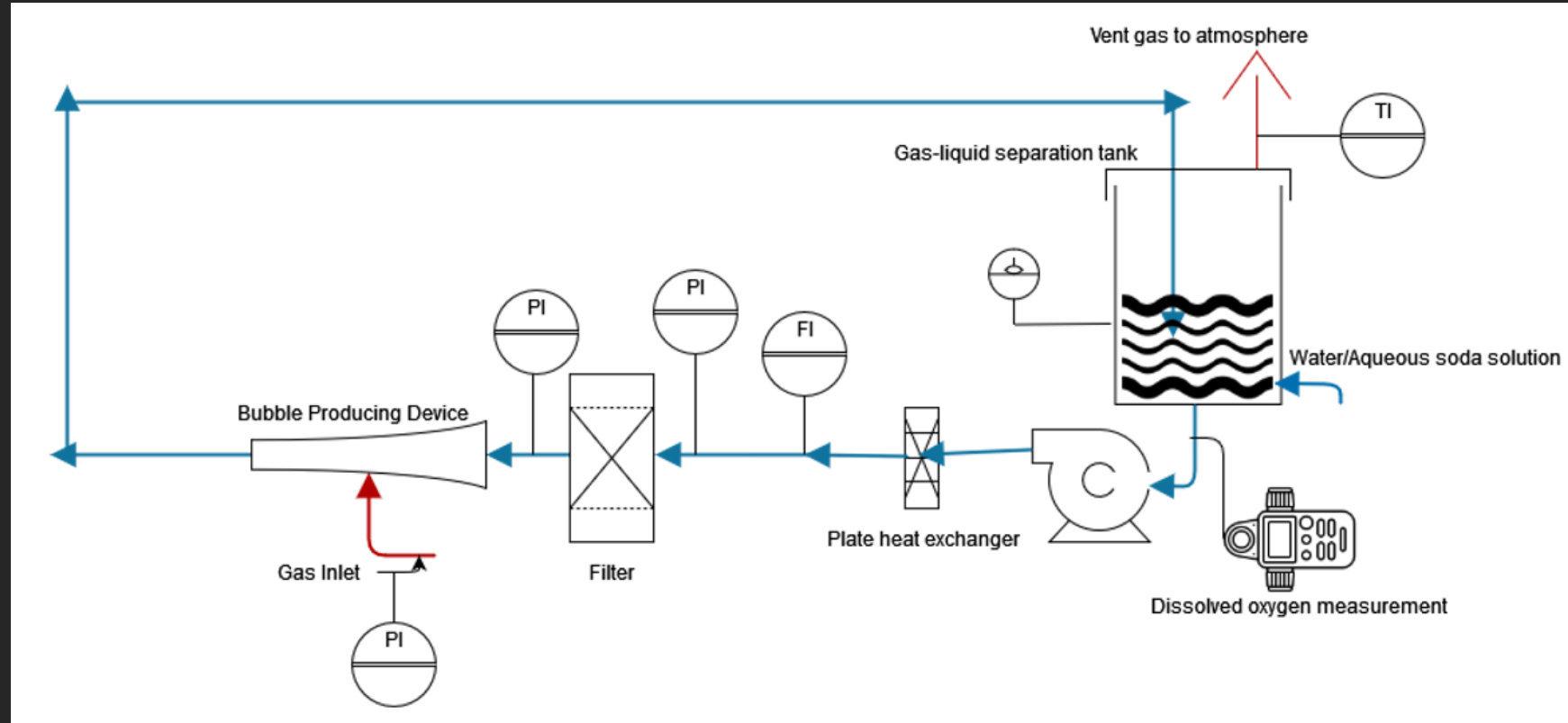
# Similar Processes

- Stockholm Exergy installed a pilot unit in Värtan's combined BECCS plant which extracts flue gases emitted out by KVV8 unit involving hot potassium carbonate technology (HPC). Capture rate was 80-95% [\[1\]](#)
- Addition of surfactant PPGME (poly propylene glycol methyl ether) into the carbonate solution to increase its absorption rate and to decrease the gas bubble size was tested in Michigan Technological university, 14 % increase in absorption rate was observed without any decrease in absorption capacity [\[2\]](#)
- Self aerated gas sparger developed by Outotec (Filters) Oy was tested and the aeration capacity, bubble sizing were measured using high speed camera, oxygenation efficiency was compared with similar systems [\[4\]](#)



# Experimental setup and Methods

- Nitrogen is purged into the system for some time and dissolved oxygen is measured until it is close to zero.
- The nitrogen valve is closed and air valve is opened, dissolved oxygen is measured.

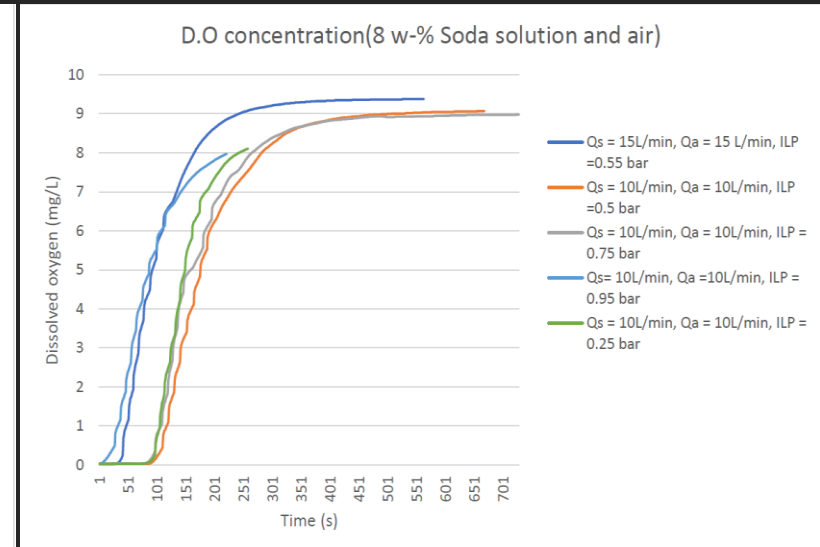
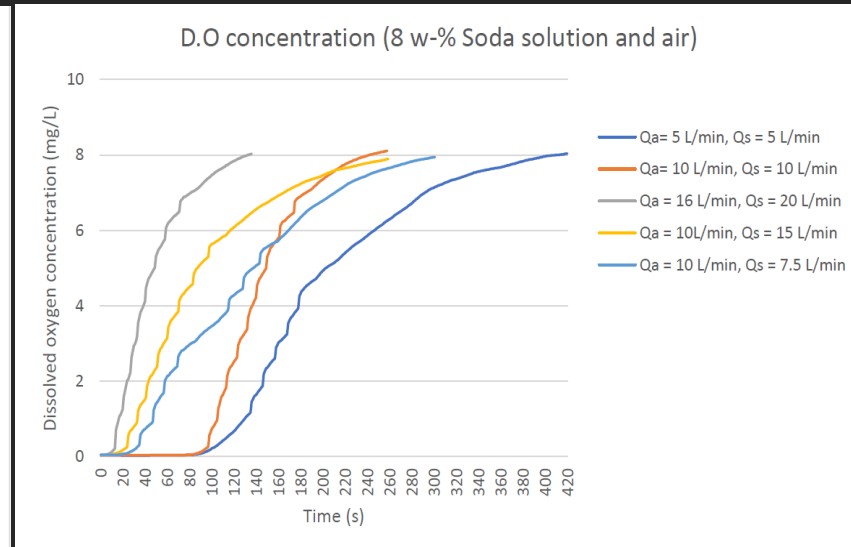
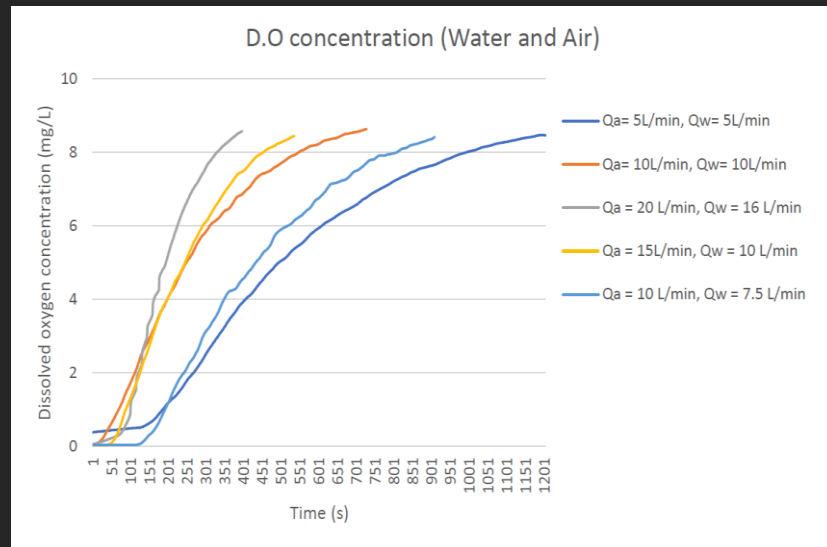




# Mass transfer rate – with no chemical reaction

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- Time lag/ response time measurements were performed for the DO probe which is used in modelling of mass transfer rate
- Dissolved oxygen concentration was measured after the gas-liquid separation tank and after the bubble producing device for water and air, 8 w-%  $\text{Na}_2\text{CO}_3$  solution and air using DO probe (YSI Pro ODO)





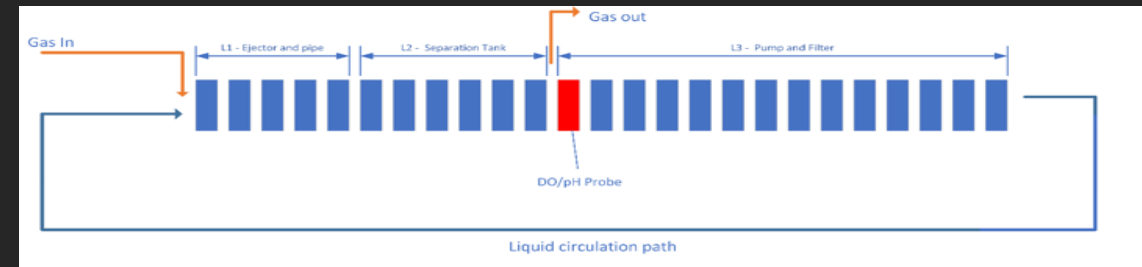
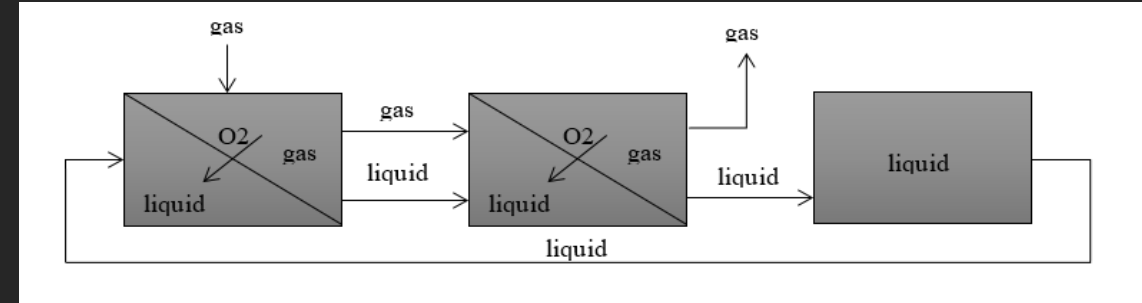
# Mass transfer rate – with no chemical reaction

$$\frac{d}{dt} C_g = -\frac{Q_g}{\epsilon_g S} \frac{d}{dx} C_g - \frac{k_L a (C_g - C_L)}{\epsilon_g S}$$

$$\frac{d}{dt} C_L = \frac{Q_L}{(1-\epsilon_g) S} \frac{d}{dx} C_L + \frac{k_L a (C_g - C_L)}{(1-\epsilon_g) S}$$

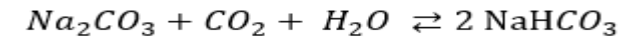
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- Diffusion of dissolved oxygen in the solution changes the concentration of oxygen in the liquid over time and distance, data fitting was performed in estimating the dynamics of oxygen changing the  $K_L a$  so that deviations between model data and measured dissolved oxygen data are minimized
- The experimental setup was assumed to be a continuous loop reactor with plug flow reactor properties
- $K_L a$  modelling was performed in MATLAB assuming no mass transfer in gas-liquid separation tank



$Q_{air}$ (L/min)	$Q_{water}$ (L/min)	$k_L a$ (1/s)
5	5	0.0054
10	7.5	0.0033
10	10	0.0113
10	15	0.0111
16	20	0.0147

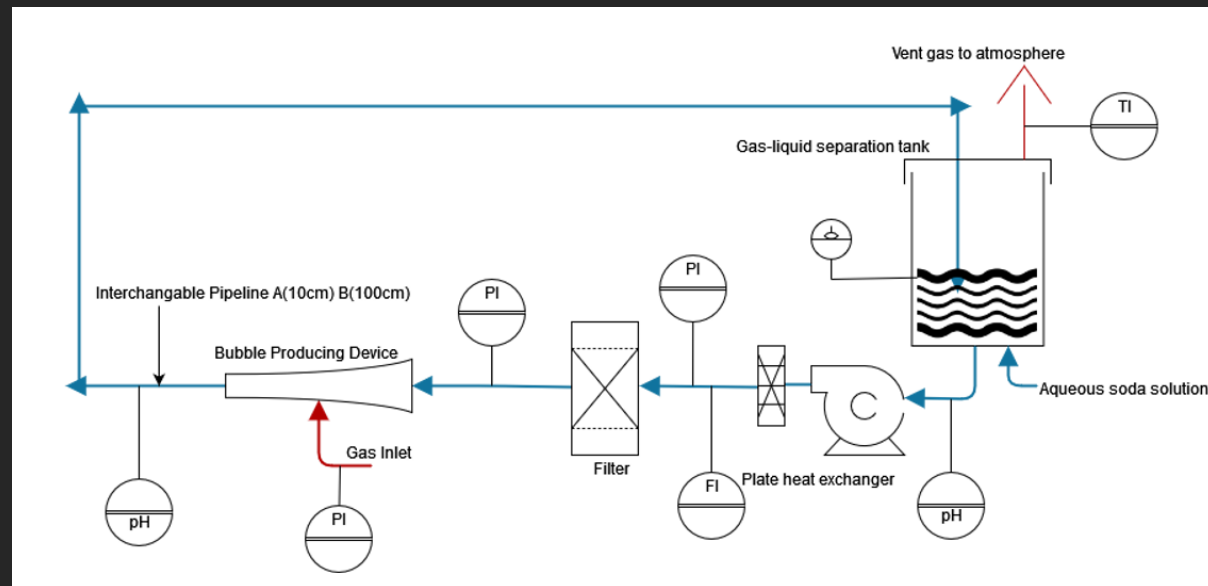
$Q_{air}$ (L/min)	$Q_{8w-\% Na_2CO_3}$ (L/min)	$k_L a$ (1/s)
5	5	0.015
10	7.5	0.0167
10	10	0.0139
10	15	0.0342
16	20	0.0634



# Mass transfer rate - with chemical reaction

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- Experimental setup was arranged in 3 ways to measure the efficiency of the system for CO<sub>2</sub> absorption using 8 w-% Na<sub>2</sub>CO<sub>3</sub> solution
- Testing with pipe A (small) and pipe B (large), testing with low liquid level in the gas-liquid separation tank using pipe A, testing with vertically mounted ejector using pipe A



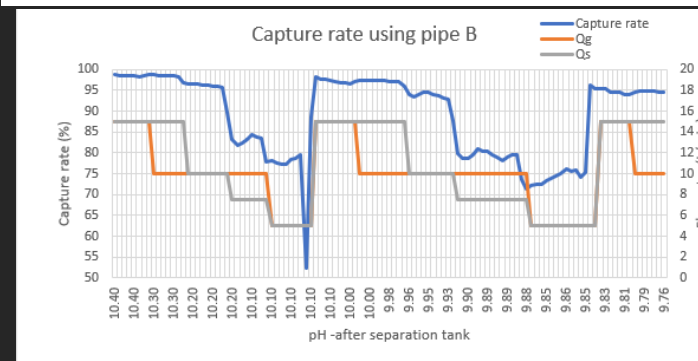
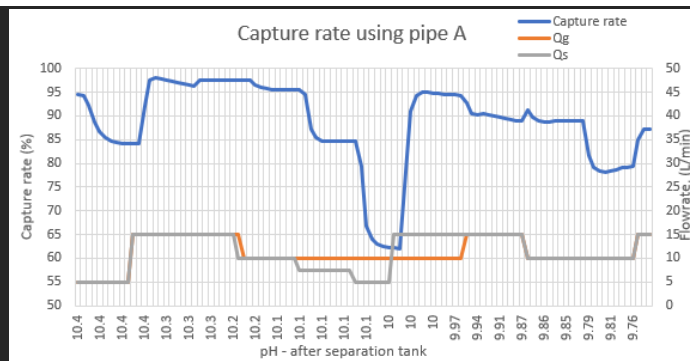
- pH was logged after the bubble producing device and after the gas-liquid separation tank, CO<sub>2</sub> lean gas was analysed and recorded



# Mass balance and capture rates

Experimental Setup	CO <sub>2</sub> in (g)	CO <sub>2</sub> out (g)	Run Time (min)	Capture rate (%)	pH – after gas-liquid separation tank
Using Pipe A (small)	571.3	44.76	149	92	11.4 – 9.76
Using Pipe B (large)	636.3	86.35	191	86	10.4 – 9.37
Low liquid level in gas-liquid separation tank	656.8	135.15	164	79	11.2 – 9.03
Vertically mounted bubble producing device	214.65	0.93	69	99	11.6 – 10.3

Experimental Setup	CO <sub>2</sub> in (g)	CO <sub>2</sub> out (g)	Run Time (min)	Capture rate (%)	pH – after gas-liquid separation tank
Using Pipe A (small)	396.81	43.09	120	89	10.4 – 9.76
/Using Pipe B (large)	381.42	34.72	111	91	10.4 – 9.76
Low liquid level in gas-liquid separation tank	220.64	26.23	62	88	10.4 – 9.76
Vertically mounted bubble producing device	40.19	0.25	17	99	10.4 – 9.76



$$CR(\%) = \frac{y(CO_2)_{in} \dot{v}_{in} - y(CO_2)_{out} \dot{v}_{out}}{y(CO_2)_{in} \dot{v}_{in}}$$





# Mass Transfer rate estimation-with Chemical reaction

- Mass transfer rate was estimated by assuming no  $\text{CO}_2$  is present in the bulk of the solution, so that the reaction is sufficiently fast. This assumption is valid by passing the condition 1
- Condition 1:  $k_L a \ll \alpha_L K_2 C_B^0$       Condition 2:  $\left[ \frac{D_A K_2 C_B^0}{k_L^2} \right] \ll 1$       There is a sufficient amount of reaction happening in film, verified by condition 2 [4]
- An excel model was developed based on the assumptions and  $K_L a$  values for corresponding flowrates was estimated using the data of vent gas mixture.

Scenario	with pipe A	Liquid mass transfer coefficient with reaction (1/s)
$Q_{gas}$ (L/min)	$Q_{liquid}$ (L/min)	
5	5	0.13
10	10	0.24
10	7.5	0.15
10	15	0.8
10	10	0.11
10	7.5	0.11
10	15	0.3

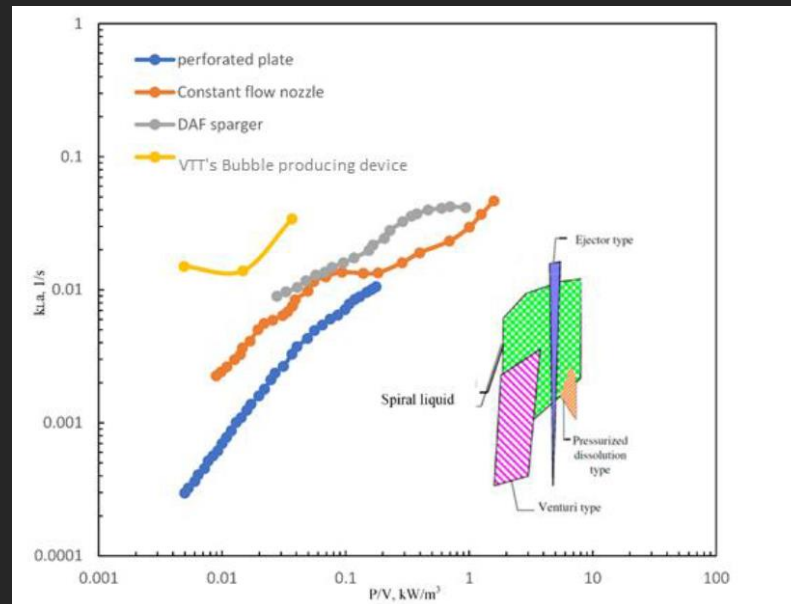
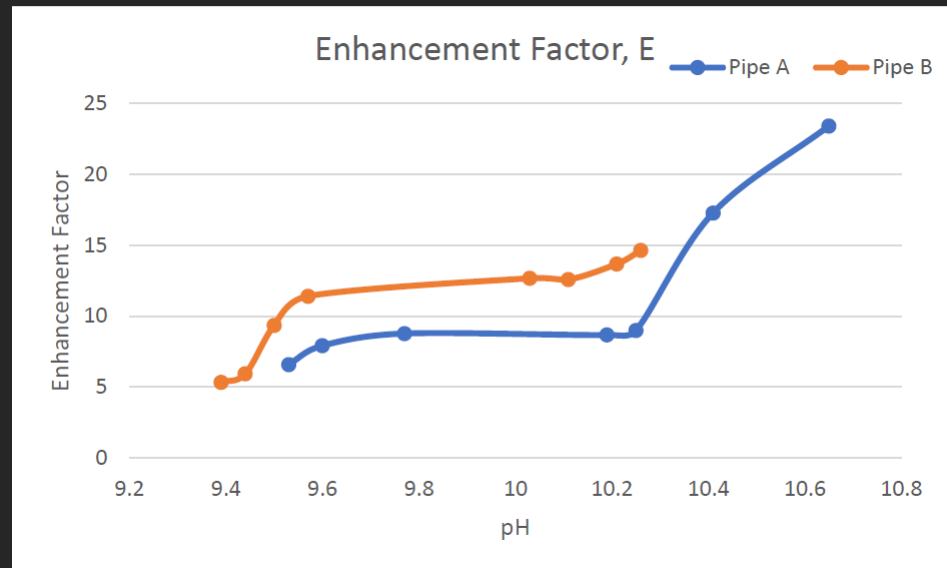
Scenario	with pipe B	Liquid mass transfer coefficient with reaction (1/s)
$Q_{gas}$ (L/min)	$Q_{liquid}$ (L/min)	
5	5	0.19
10	10	0.19
10	7.5	0.21
10	15	0.5
5	5	0.08



# Enhancement and Pumping Energy Input

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- Enhancement Factor, by comparing the mass transfer rate with reaction and without reaction. Mass transfer is enhanced by roughly 10 times due to chemical reaction happening around a pH 10 in the solution
- VTT's bubble producing device is in a bit higher position in terms of mass transfer efficiency as a trade off for pumping energy input



Adopted from : Dmitry Gradov, Auto-Aspirated DAF Sparger Study on Flow Hydrodynamics, Bubble Generation and Aeration Efficiency, 2021

29.06.2023



# Conclusions & Remarks

- L/G ratio appears to be more important since it affects the mass transfer, ideal L/G ratio and residence time will be 1.25 (8 w-%  $\text{Na}_2\text{CO}_3$  solution =15L/min, synthetic gas mixture 10L/min) and
- Pipe A (short pipe) is more efficient than pipe B (longer pipe) since in pipe B bubbles start to agglomerate soon and mass transfer is limited
- With soda solutions due to chemical reaction absorption is enhanced approximately 10 times
- Commercializing of this VTT's novel soda process was started by Kleener Power Solutions Ltd.

# Acknowledgements



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- My sincere thanks to Dr. Kristian Melin (Assistant professor, LUT University) Tuula Kajolinna,, VTT (Technical Research Centre of Finland) for providing a conducive atmosphere to experiment and learn.
- In the photo: Test group of VTT and LUT at the test facilities in VTT Espoo, August 2021. Persons in the picture are Mohankumar Narayanasamy (LUT), Tuula Kajolinna (VTT), Kristian Melin (LUT), Andrey Saren (LUT) and Johannes Roine (VTT). Picture: VTT



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- Gradov, D.V.; Saren, A.; Kauppi, J.; Ullakko, K.; Koironen, T. Auto-Aspirated DAF Sparger Study on Flow Hydrodynamics, Bubble Generation and Aeration Efficiency. *Processes* **2020**, *8*, 1498. <https://doi.org/10.3390/pr8111498> [4]



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- Mandal, A. et al(2003) Interfacial Area and Liquid-Side Volumetric Mass. Canadian Journal of Chemical Engineering, Volume 81, pp. 212-218 [5]



Thanks for listening!

Questions?

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Blog from VTT: <https://www.vttresearch.com/en/news-and-ideas/novel-eco-friendly-technology-capture-co2>